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Title:	Linearized three-phase optimal power flow models for distribution grids
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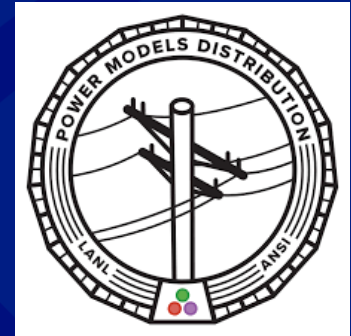
Linearized Three-Phase Optimal Power Flow Models for Distribution Grids

Presented by: Kshitij Girigoudar

Mentors: David Fobes & Russell Bent

Student Lightning Talks

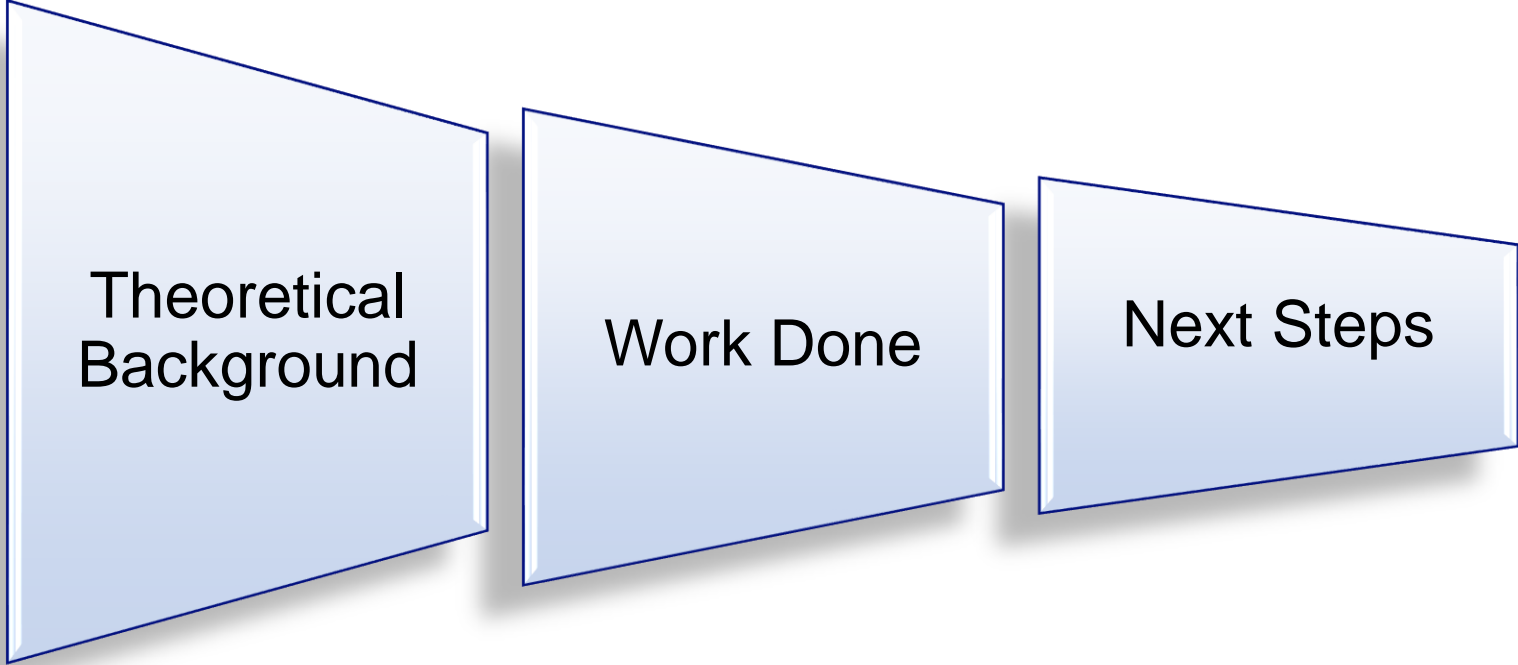
10 August 2021



About me

- **Current education:** Fourth year PhD student at University of Wisconsin-Madison
- **Research interests:** Optimization and control of power systems
- **Hobbies:** Hiking, video games, badminton and chess

Outline



Theoretical
Background

Work Done

Next Steps

Outline

Theoretical Background

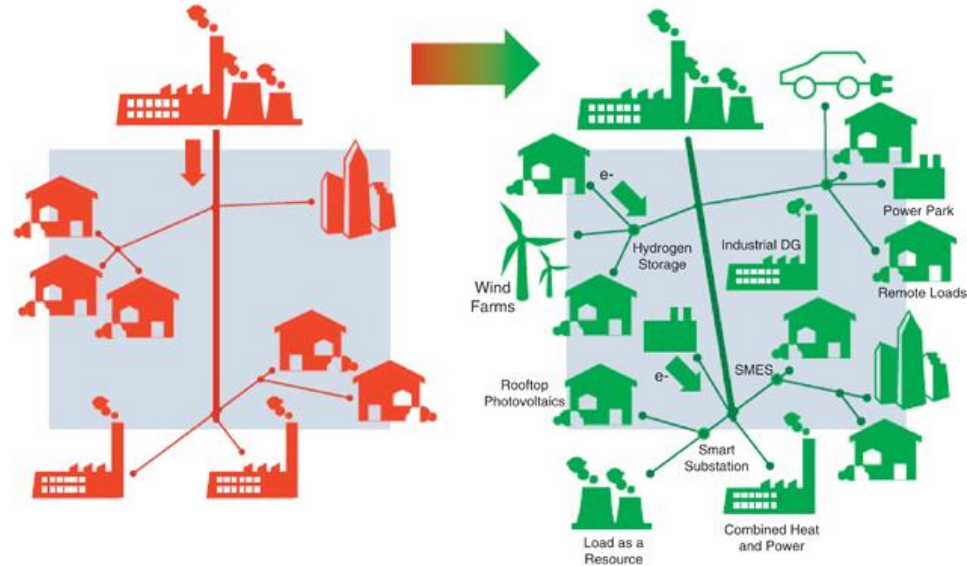
- Distribution Grids
- Optimal Power Flow

Work Done

Next Steps

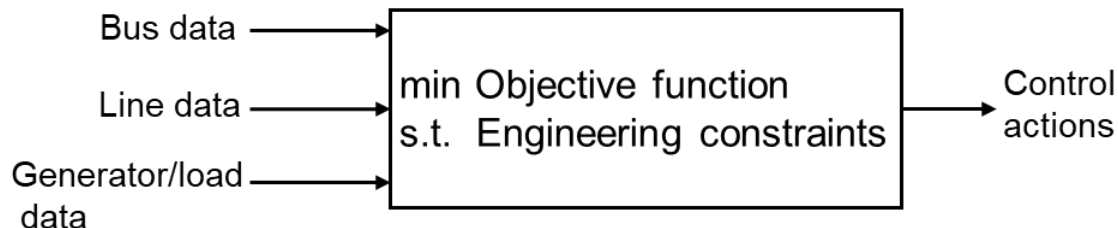
Distribution Grids

- Interconnection between transmission grid and end consumers
- Characteristics different from transmission grid
 - Distributed energy resources (DERs)
 - Radial or near radial structure
 - Unbalanced three-phase systems
 - Untransposed lines with high R/X ratio
 - Asymmetrical loads



Optimal Power Flow (OPF)

- Optimization problem **solving power flow** while also **optimizing** operating conditions and **adjusting** control actions

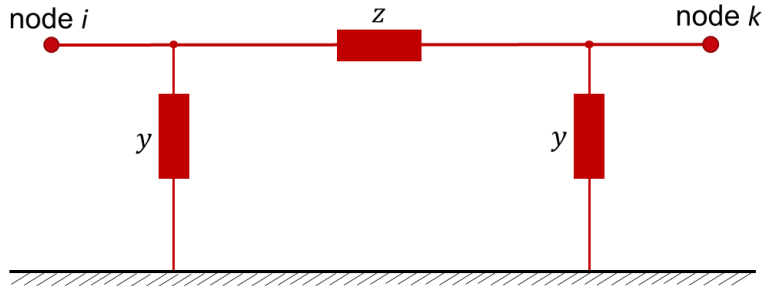


- **PowerModelsDistribution.jl**- Julia package for steady-state distribution grid optimization
 - **PowerModels.jl**- steady-state transmission grid optimization



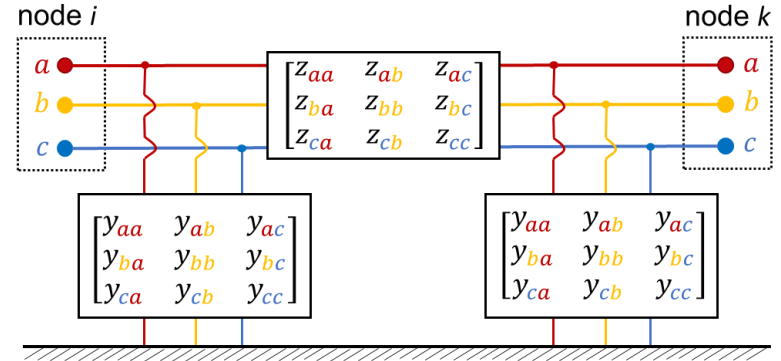
PowerModels vs PowerModelsDistribution

Transmission line



- Balanced system

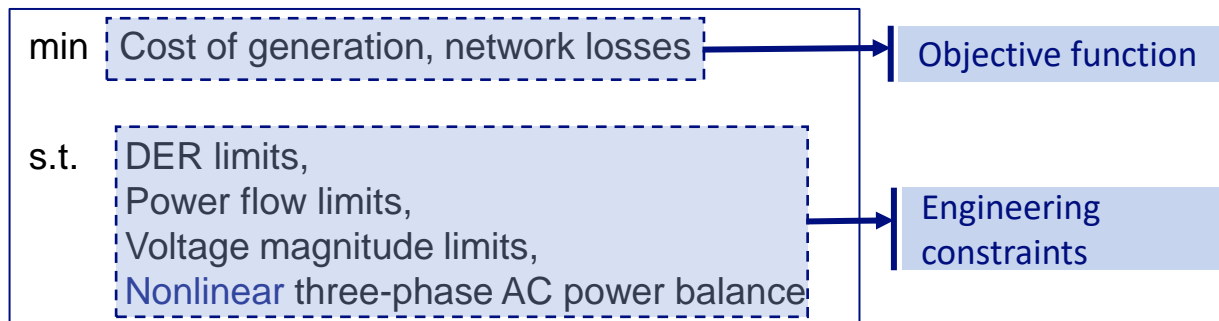
Distribution line



- Unbalanced system with interphase coupling

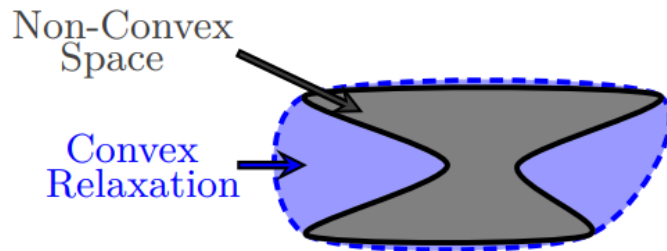
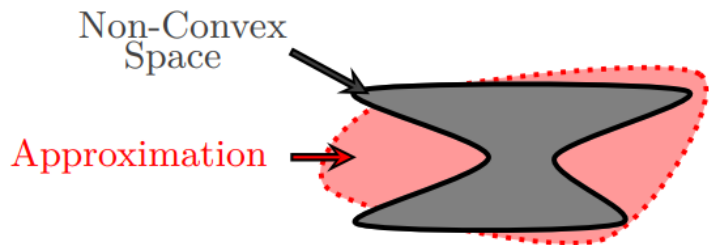
Three-phase Optimal Power Flow

- Nonlinear, nonconvex optimization problem solved using Ipopt



- Problem:** Challenging to solve for large, realistic distribution grids ☹️
- Solution:** Reduce computational complexity using approximations/relaxations 😊

Approximations vs Relaxations



Molzahn, Daniel K., and Ian A. Hiskens. "A survey of relaxations and approximations of the power flow equations." *Foundations and Trends® in Electric Energy Systems* 4.1-2 (2019): 1-221.

- Does not enclose non-convex feasible space
- More computationally tractable
- Example: LinDistFlow

- Enclose non-convex feasible space
- Inefficient scaling for large systems
- Restrictions on possible objectives
- Example: SDP, SOC

Outline



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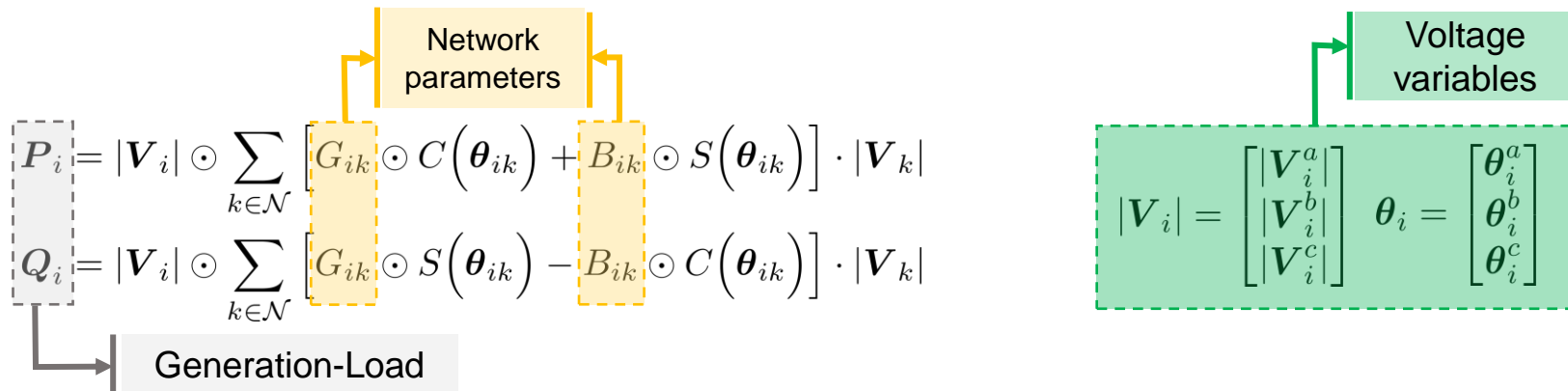
Work Done

- Linear
Approximations

Next Steps

Nonlinear AC Power Balance Equations

- Satisfy **power balance** at all nodes (polar coordinate frame)



$$C(\theta_{ik}) = \begin{bmatrix} \cos(\theta_i^a - \theta_k^a) & \cos(\theta_i^a - \theta_k^b) & \cos(\theta_i^a - \theta_k^c) \\ \cos(\theta_i^b - \theta_k^a) & \cos(\theta_i^b - \theta_k^b) & \cos(\theta_i^b - \theta_k^c) \\ \cos(\theta_i^c - \theta_k^a) & \cos(\theta_i^c - \theta_k^b) & \cos(\theta_i^c - \theta_k^c) \end{bmatrix}$$

$$S(\theta_{ik}) = \begin{bmatrix} \sin(\theta_i^a - \theta_k^a) & \sin(\theta_i^a - \theta_k^b) & \sin(\theta_i^a - \theta_k^c) \\ \sin(\theta_i^b - \theta_k^a) & \sin(\theta_i^b - \theta_k^b) & \sin(\theta_i^b - \theta_k^c) \\ \sin(\theta_i^c - \theta_k^a) & \sin(\theta_i^c - \theta_k^b) & \sin(\theta_i^c - \theta_k^c) \end{bmatrix}$$

First-order Taylor (FOT) Approximation

- Linearized power balance equations

$$\begin{bmatrix} P \\ Q \end{bmatrix} = \begin{bmatrix} P_0 \\ Q_0 \end{bmatrix} + J_0 \cdot \begin{bmatrix} |V| - V_0 \\ \theta - \theta_0 \end{bmatrix}$$

The diagram illustrates the First-order Taylor (FOT) Approximation for power balance equations. The equation shows the vector $\begin{bmatrix} P \\ Q \end{bmatrix}$ as the sum of the initial operating point $\begin{bmatrix} P_0 \\ Q_0 \end{bmatrix}$ and the product of the Jacobian J_0 and the deviation from the initial operating point $\begin{bmatrix} |V| - V_0 \\ \theta - \theta_0 \end{bmatrix}$. The initial operating point is highlighted in a blue dashed box, and the Jacobian J_0 is highlighted in a green dashed box. A green arrow points from the Jacobian box to the word "Jacobian" in a green box. A blue arrow points from the initial operating point box to the text "Initial operating point" in a blue box.

$$J = \begin{bmatrix} \frac{\delta P}{\delta |V|} & \frac{\delta P}{\delta \theta} \\ \frac{\delta Q}{\delta |V|} & \frac{\delta Q}{\delta \theta} \end{bmatrix}$$

Forward-Backward Sweep (FBS)

- Backward Sweep (KCL)

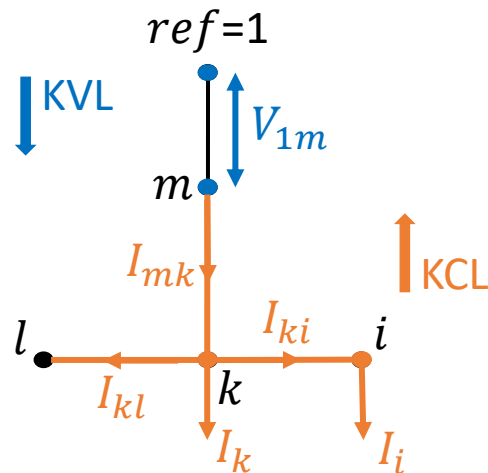
$$I_i = I_{ki} = \frac{(P_i - jQ_i)}{\bar{V}_{i0}}$$

Initial operating point

$$I_{mk} = I_k + \sum_{n \in \{i, l\}} I_{kn}$$

- Forward Sweep (KVL)

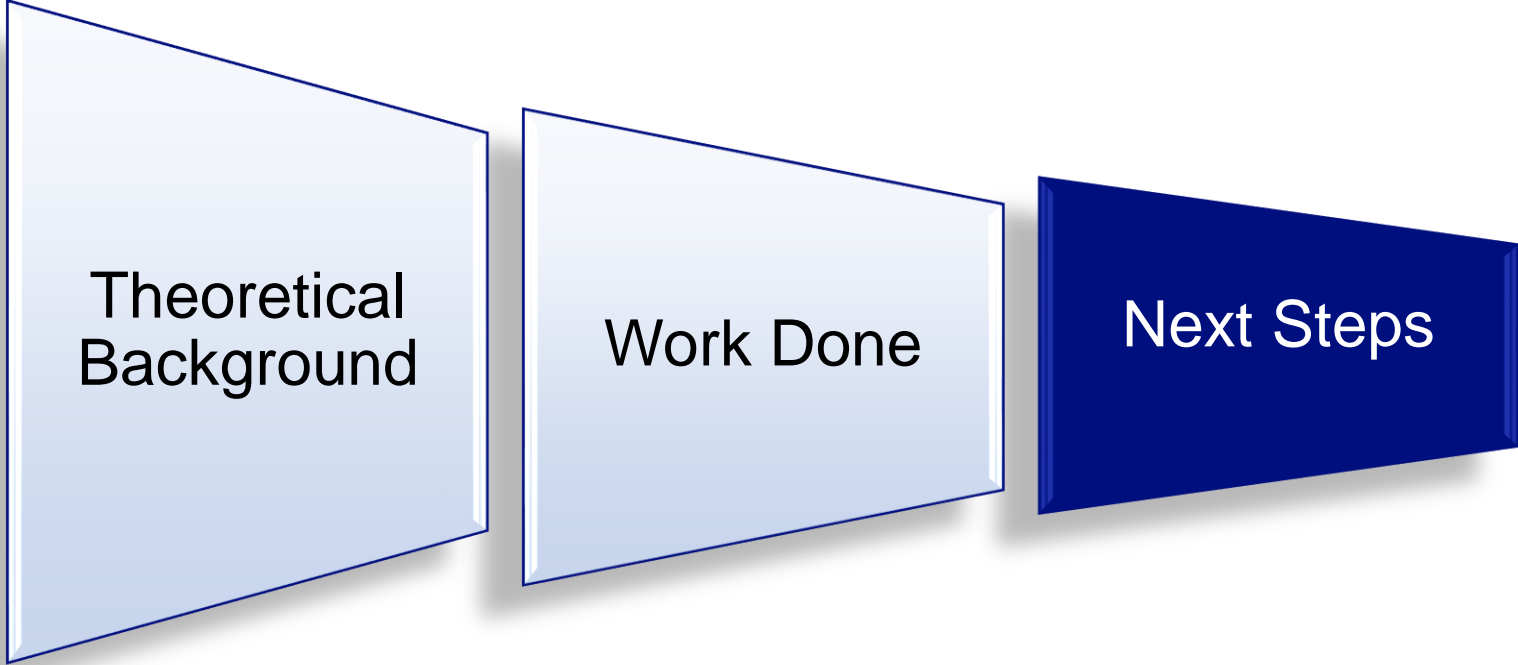
$$V_m = V_1 - \underbrace{Z_{1m} \cdot I_{1m}}_{V_{1m}}$$



Summary

Method	Advantages	Limitations
Three-phase OPF	Converges to AC feasible solution	Large computation time
FOT-OPF	Best local approximator	Jacobian calculation can be time-consuming
FBS-OPF	Faster than FOT since it exploits radial topology	Less accurate compared to FOT

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Next Steps

Next Steps

- Testing performance of linear approximations on large, realistic distribution grids
 - Compare solution accuracy and computation time
 - Use different initial operating points
- Warm-starting three-phase OPF to check for improvement in computation time

Thank you for your attention!



With great **power** comes great **responsibility** ...

... and greater **electricity bill** !!

Questions